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FATIGUE TEST OF
THE MAIN ROTOR RETENTION COMPONENTS
USED ON MODEL OH-58A/206A-1 HELICOPTER
(P. I. P. TASK 69-29)

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PREPARED BY

BELL HELICOPTER COMPANY

FORT WORTH, TEXAS 76101



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TECHNICAL DATA

BY *R. Amancharla* DATE April 30, 1971
R. Amancharla
CHECKED *J. K. Sen* DATE April 30, 1971
J. K. Sen
APPROVED *G. L. Rodriguez* DATE April 30, 1971
G. L. Rodriguez
APPROVED *George H. Tinnabery* DATE April 30, 1971
G. H. Tinnabery, Chief
Engineering Laboratories

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RETENTION COMPONENTS USED ON
MODEL OH-58A/206A-1 HELICOPTER

PREPARED UNDER CONTRACT DAAJ01-70-C-0057(2E)
P.I.P. TASK 69-29

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3. Bell Drawing No. 206-010-105, "Strap Assembly, Tension Torsion, Main Rotor."
4. Bell Drawing No. 206-010-123, "Pin-Strap Retaining, Main Rotor."
5. Bell Drawing No. 206-010-155, "Fitting-Retention Strap, Main Rotor, Assembly of."
6. Bell Drawing No. 206-010-169, "Bolt-Strap Retaining, Main Rotor."
7. Bell Engineering Order 206HA86, "To Provide Parts for Fatigue Test."
8. Bell Drawing No. 299-098-015, Sheet 5, "Fatigue Machine for Model 206 Main Rotor Blade Retention Strap."
9. Bell Engineering Laboratories Notebook No. N70-25.
10. Bell Report No. 206-099-114, "Fatigue Life Substantiation for the Dynamic Components of Model 206A-1 Helicopter."
11. Bell Engineering Order 206HA1818, "Rework the Test Specimen Used in the Fatigue Test of OH-58A/206A-1 Main Rotor Retention Components."

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INTRODUCTION

This report presents the results of a fatigue test conducted on eight sets of main rotor retention components used in the main rotor hub assembly of the Model OH-58A/206A-1 helicopter, Ref. 1. The test was conducted to justify an extension of the recommended service life of the retention components. The fatigue test was conducted in accordance with Ref. 2, except for a subsequent addition in the test program. A total of eight sets of components were tested as against the four sets specified.

Each set of the components tested consisted of one 206-010-105-3 strap assembly, Ref. 3, Fig. 1, one 206-010-123-1 pin, Ref. 4, Fig. 2, and one 206-010-155-7 or 206HA86-1 fitting, Ref. 5 and 7, Figs. 3 and 4. In the last four sets tested the -155-7 fittings were replaced by the 206HA86-1 fittings, Ref. 7, Fig. 4. The 206HA86-1 fitting, Ref. 7, is the same as the -155-7 fitting except that the 45 degree angular cuts were deleted. In each set tested, one new 206-010-169-1 strap retaining bolt, Ref. 6, was used as a supporting part, Fig. 5. A detailed description of all the test parts is given under Test Specimen section.

The strap assemblies are used in the main rotor hub assembly, Ref. 1, to transmit the main rotor centrifugal load to the 206-010-101-9 yoke assembly. The strap assembly is designed to be flexible in torsion in order to permit pitch change of the rotor blade during helicopter operation. It is located along the pitch change axis between the main rotor yoke and grip assembly.

The fittings are located along the pitch change axis inside the yoke assembly and accept the inboard end of the strap assembly. The pin locks the strap assembly in the fitting. The outboard end of the strap assembly is accepted by a pair of tangs in the grip assembly, and is locked in by a retaining bolt.

Each of the eight sets of components tested were subjected to mean and oscillatory angular twist and centrifugal loads based on the loads specified in Ref. 2. The test was conducted in two phases. During the first phase each set of the components were subjected to an oscillatory twist

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loading with a steady axial load which simulated the centrifugal force. During the second phase the components were subjected to start-stop cycle loading which simulated the starting and stopping of the helicopter. The angular twist loads in degrees are specified with reference to the angular twist of the strap assembly. A detailed description of the loads is given under Test Loads.

The testing of the components was accomplished using a test machine designed especially for this purpose, Ref. 8. The test setup is shown in Figs. 6, 7, and 8. In the test setup, two sets of components were tested simultaneously utilizing actual helicopter components wherever possible. The eight sets of components were tested in a sequence of four tests. The axial load simulating centrifugal force was applied with a hydraulic cylinder. The start-stop cycling was accomplished by cycling the hydraulic cylinder with a four way valve. Each strap assembly was pretwisted at the inboard end, and the desired oscillatory twist applied at the outboard end by means of an eccentric driven by an electric motor. Each component of a test set was removed from the test machine after a predetermined number of test cycles and inspected for failure. The inspection cycle intervals and a detailed description of the test setup are presented in Apparatus and Methods.

All the test data is recorded in Ref. 9. The test was conducted in the Mechanical Test Laboratory of Bell Helicopter Company, Fort Worth, Texas between Sept. 9, 1970 and Jan. 15, 1971.

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RESULTS

A summary of the fatigue test results for the eight sets of main rotor retention components is given in Tables I through III. Photographs of the condition of the retention components and supporting parts are given in Figs. 9 through 16.

Each set of the retention components was first subjected to ten million cycles of oscillatory twist of 20 ± 14 degrees combined with a steady axial load of 44,000 lbs. Following the oscillatory twist loading, each set of components was subjected to a 34,500 start-stop cycle test, during which the axial load was varied from 0 to 44,000 lbs. at 14 cycles per minute with a steady twist of 23 degrees. During the oscillatory twist phase of testing, there were no failures of any components. All failures occurred during the start-stop phase of the test.

There were no failures of the eight 206-010-105-3 strap assemblies tested. However, two straps were damaged by compressive buckling as a result of a test machine failure and one strap was damaged due to a 206HA86-1 fitting failure.

Nine of the ten -123-1 pins were tested without failure. One -123-1 pin indicated fatigue failure after 34,568 start-stop cycles.

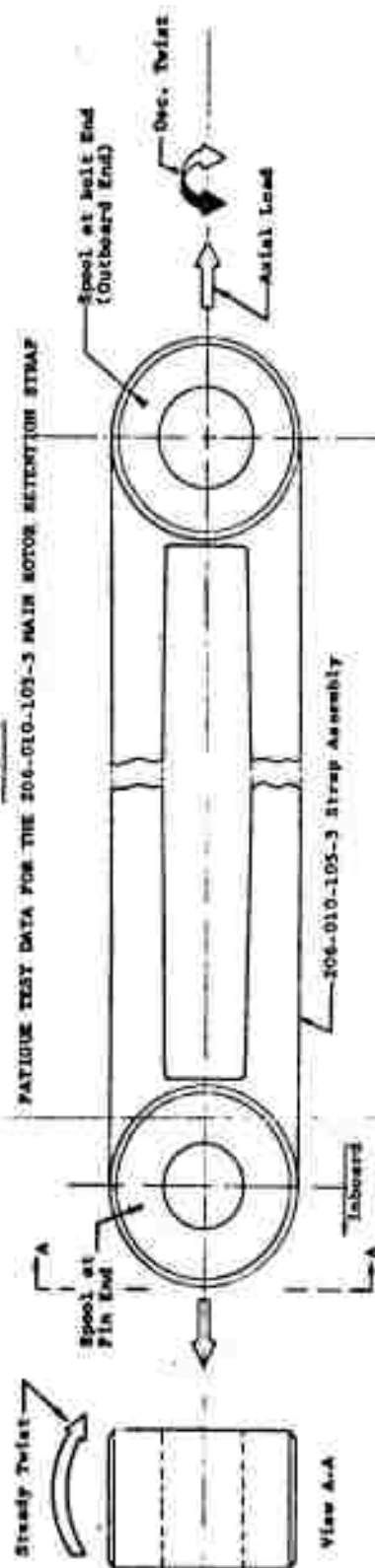
Each of the four -155-7 fittings tested indicated fatigue cracks after completing 13,000 start-stop cycles, but each part continued to react axial load. The four 206HA86-1 fittings used to replace the -155-7 fittings completed the required 34,500 start-stop cycles without failure.

At the end of the test program, the start-stop phase of the test for the last two sets of the retention components with the 206HA86-1 fittings was continued until a failure occurred. After 72,326 start-stop cycles, the 206HA86-1 fitting, ML-4, used with strap specimen No. 8 failed as shown in Fig. 14. The -1 fitting, ML-3, used with set No. 7, showed fatigue cracks at the pin hole as shown in Figs. 14 and 16.

Test results of each retention components are discussed in detail under Discussion of Results.

TABLE I

PATRIQUE TEST DATA FOR THE 206-C10-103-3 MAIN MOTOR RETENTION STRAP



Test No.	Strap Specimen No.	Serial No.	Type of Loading in Sequence	Test Loads		Applied Test Cycles	Summary of Results	Ref. Fig. No.
				Twist Start-Stop	Static Load			
1	1	1447	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 34,538	No failure No failure. Light to medium fretting on end spool faces. Δ	10
2	2	1453	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 34,538	No failure. No failure. Fretting on end spools same as above. Δ	11
3	3	6003	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 20,292	No failure. No failure. Light to medium fretting on end spool faces. Test discontinued due to the damage caused by test machine failure.	9
4	4	6023	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 20,292	No failure. Result similar to specimen No. 3.	9
5	5	6027	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 34,523	No failure. No failure. Medium fretting on spool faces. The webboard and wires heavier fretting.	10
6	6	6054	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 34,533	No failure. No failure. Fretting condition similar to specimen No. 5.	10
7	7	6088	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 22,216	No failure. No failure. Fretting conditions were the same as for specimen No. 5.	11
8	8	6111	Twist Start-Stop	14 None	44,000 0 to 44,000	10,000,000 22,216	No failure. After 34,540 cycles there were no failure. Fretting was similar to specimen Nos. 5 and 6. After 72,326 cycles, the straps were damaged when the 20N4445-3 fitting failed.	11

Δ Test machine failed after 24,291 start-stop cycles, but test was continued.

△ Test machines failed after 24,381 start-drop cycles, but test was continued.

TABLE 11

FATIGUE TEST DATA FOR THE 205-010-123-1 MAIN MOTOR RETENTION STRAP RETAINING PIN

Test No.	Strap Specimen No.	Pin Specimen No.	Test Loads			Applied Test Cycles	Summary of Results
			Type of Loading in Sequence	Twist Angle in Degrees	Axial Load in Pounds		
1	1	Q1-2289	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
2	2	Q1-2284	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
3	3	Q1-2277	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
4	4	Q1-2285	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
5	5	Q1-2277	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
6	6	Q1-2277	Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.
			Twist Start-Stop	20 23	14 None	10,000,000 34,568	No failure. Medium fretting on contact areas.

NOTES: Δ Test loads are same as listed for the corresponding -109-3 retention straps in Table 1.

Δ Pin specimen Nos. 3 and 6 were used with re-worked -135-7 fittings, Ref. 11, and were used in place of pin specimen Nos. 2 and 4 to continue the test.

Δ The new fittings, P/N 201148-1, were used with specimen Nos. 7 through 10.

TABLE III (Continued)

Test No.	Strap Spec. No.	Fitting Specimen No. and Part No.	Fitting Serial No.	Type of Loading	A Test Loads		Applied Test Cycles	Summary of Results
					Twist Angle, Degrees	Axial Load in Pounds		
2	1, 3	Δ 5 -155-7	ML-1	Start-Stop	23	None	28,000	Failed at all the four corners. Crack location similar to earlier cracks after 13,175 cycles.
	2, 4	Δ 6 -155-7	ML-2	Start-Stop	23	None	28,000	Fatigue cracks found at all four corners similar to specimen No. 5, but the breakwires did not break.
3	5	1 206HA86-1	ML-1	Twist Start-Stop	20 23	14 None	10,000,000 34,525	No failure.
	6	2 206HA86-1	ML-2	Twist Start-Stop	20 23	14 None	10,000,000 34,525	No failure. Minor fretting at the hole and innerface. Ref. Fig. 14.
4	7	3 206HA86-1	ML-3	Twist Start-Stop	20 23	14 None	10,000,000 72,326	No failure.
	8	4 206HA86-1	ML-4	Twist Start-Stop	20 23	14 None	10,000,000 72,326	Failed at the pin hole. There were no failures when inspected last at 34,500 cycles. Ref. Fig. 14.
								No failure.
								Failed circumferentially across the hole. There were no failures when inspected after 34,500 cycles. Ref. Fig. 15 and 16.

NOTES: Δ These two fittings were modified per and identified by E.O. 206HES1818, Ref. 11. The modification consisted of increasing the corner radii at the location of failures noted in specimen Nos. 1 through 4 and shot peening the re-machined surfaces. These were used only for start-stop cycles and were not subjected to twist cycles.

Δ Test loads are as applied on the corresponding -105-3 retention strap.

Δ The fittings in test Nos. 2, 3, and 4 were breakwired at possible locations of failure to stop the test machine in case of a fitting failure.

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DISCUSSION OF RESULTS

All the test parts used in the eight sets of retention components completed ten million oscillatory twist cycles without any failure. All the failures noted herein occurred during the start-stop cycle tests.

One new 206-010-169-1 strap retaining bolt, Fig. 5, was used in each set of retention components as a supporting part. None of the -169-1 bolts used in the test indicated any failure. At the end of the test all the test parts were subjected to metallurgical examination. All the failed parts were checked and found to be within corresponding blueprint requirements except the -155-7 fitting, S/N J11-2070. The metallurgical examination results on this fitting are given under discussion of results of the -155-7 fitting.

A brief discussion of each component tested is given below:

206-010-105-3 Retention Strap

A summary of the fatigue test results on eight -105-3 strap assemblies is given in Table I. Specimen Nos. 1 through 4 were tested with the -155-7 fittings and specimens Nos. 5 through 8 were tested with the 206HA86-1 fittings. The eight specimens completed 10⁷ cycles of oscillatory twist loading without failure.

During the test for start-stop cycles, the six straps, specimen Nos. 1, 2, 5, 6, 7 and 8 completed 34,500 cycles without failure. Inspection of the specimens 1 and 2 after 34,568 cycles revealed a slight bulge near the ends, which was the damage caused due to the failure of a hydraulic cylinder in the test machine after 24,291 cycles of testing. The resulting shock load buckled the straps, but the damage did not adversely affect the test results.

Two straps, specimen Nos. 3 and 4, completed 20,292 start-stop cycles without failure but testing was stopped because the straps were severely buckled in compression, Fig. 9, as a result of a second hydraulic cylinder failure which resulted in a high compressive shock load.

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Strap specimen Nos. 5 and 6 completed 34,525 cycles without failure, and specimen Nos. 7 and 8 completed 72,326 cycles without failure. The inboard end of strap specimen No. 7 was damaged, as shown in Fig. 11, due to the failure of corresponding -86-1 strap fitting, Specimen ML-4, after 72,326 cycles, Fig. 15.

At the conclusion of each test, light to medium fretting was found on the faces of the end spools. In general, the spool at the inboard end, which attached to the -155-7 fitting, showed less fretting than the spool at the outboard end. Typical fretting conditions of the straps after 20,292 cycles, 14,000 cycles and 72,326 cycles are shown in Figs. 9, 10, and 11, respectively. The amount of fretting noted did not have any significant effect on the fatigue test results.

206-010-123-1 Strap Retaining Pin

A summary of the test results on ten -123-1 pins is presented in Table II.

Eight of the ten pins used were subjected to 10^7 oscillatory twist cycles and then the start-stop loading cycles as discussed below. Two of the ten pins were subjected to only start-stop cycles because they were used to complete a block of 34,500 start-stop cycles on strap specimen Nos. 3 and 4.

Five of the eight pins subjected to 10^7 twist cycles also completed the required block of 34,500 start-stop cycles without failure. Two other pins completed 10^7 twist cycles and 13,411 start-stop cycles without failure. Testing was stopped at 13,411 cycles because of failure of the -155-7 fittings.

One of the eight pins, specimen No. 2, subjected to 10^7 twist cycles and 34,568 start-stop cycles was found to have a fatigue crack upon inspection after completion of 34,568 start-stop cycles. The fatigue crack originated in a heavily fretted area, Fig. 12. This pin was used with two -155-7 fittings during the test. The original -155-7 fitting was found to contain fatigue cracks after 13,400 start-stop cycles and a new fitting identified as Part No. 206HES-1818-1 was installed to complete the 34,568 cycles on the strap and pins.

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The magnitude of the fretting was heavy on the bearing surfaces of all ten pins tested. However, no significant difference in fretting was apparent because of replacing the -155-7 fittings with the 206HA86-1 fittings.

206-010-155-7 and 206HA86-1 Retention Strap Fittings

A summary of the test data and results of six -155-7 and four 206HA86-1 fittings are given in Table II. All of the four -155-7 fittings, specimen Nos. 1 through 4, successfully withstood 10⁷ cycles in twist loading without any failure. Specimen Nos. 5 and 6 were not subjected to any oscillatory twist loading.

During the start-stop cycle test, each of the four fittings, specimen Nos. 1 through 4, showed fatigue cracks at the top corners of the rectangular cavity after 13,400 cycles, Fig. 13. The fatigue cracks were located at all of the four corners for three specimens, the crack-lengths varying from 1/8 to 3/8 of an inch. The fourth specimen, S/N J11-2098, had fatigue cracks at three of the four corners. The first inspection on specimen Nos. 1 and 2 was conducted after 13,400 start-stop cycles, and hence the exact number of cycles to failure was not known. During the test specimen Nos. 3 and 4 were breakwired on the possible locations of failure to stop the test machine in the event of a fitting failure. The breakwire on specimen No. 3, S/N J11-2098, failed after 6550 cycles. Inspection of specimen No. 3 after 13,411 cycles, revealed fatigue cracks at three corners of the fitting. The longest crack was located at the location of the breakwire failure. Since the breakwire was open at this place after 6550 cycles, specimen No. 3 is considered to have failed after 6550 start-stop cycles.

Specimen No. 4 fitting, S/N J11-2111, did not show any breakwire failure, though during the inspection after 13,411 cycles it showed fatigue cracks at all four corners.

The metallurgical examinations of all the -155-7 fittings revealed that all the fatigue cracks origins were located at the chamfered radii of the corners. Typical origin and extent of fatigue crack is shown in Fig. 13. The material properties of all fittings was checked subsequent to test and found to be within blueprint specification except for fitting S/N J11-2070.

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The metallurgical examination of the -155-7 fitting, S/N J11-2070, indicated a surface heat treat of 214,000 psi, tensile, which is above the blueprint requirement of 180,000 - 200,000 psi, tensile. Chemical analysis revealed that the carbon content is higher on the surface than the core. The core was found to be at C42 on Rockwell Scale, which corresponds to a heat treat of 194,000 psi tensile.

Following the failures of the -155-7 fittings, two -155-7 fittings, specimen Nos. 5 and 6 were modified by Engineering Order 206HES1818, and used to complete the required number of start-stop cycles on strap specimen Nos. 1 through 4.

The four 206HA86-1 fittings used with strap specimen Nos. 5 through 8 completed 10⁷ twist cycles followed by 34,520 start-stop cycles without any failure. The test of specimen Nos. 7 and 8 were continued past the 34,520 start-stop cycles, until a failure occurred at 72,326 cycles. After 72,326 cycles the 206HA86-1 fitting, ML-4, with strap specimen No. 8 failed at the hole as shown in Figs. 15 and 16. At the conclusion of the test, the fitting used with strap specimen No. 7, ML-3, also showed fatigue cracks at the inside corners of the pin hole, Figs. 14 and 16. Typical areas and extent of fretting are given in Fig. 14.

The metallurgical examination of the failed 206HA86-1 fittings indicate that all the fatigue origins were located at the inside chamfer radius of the pin hole in the fitting.

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CONCLUSIONS

Based on the test results reported herein, it is concluded that the 206-010-155-7 is the weakest of the main rotor strap components and did not meet the specified requirements for an increase in fatigue life. However, the 206HA86-1 fitting that replaced the -155-7 fitting did meet the specified requirements for an increased service life.

Final conclusions and recommendations as to the service life of the retention components tested will be the subject of another report, Bell Report 206-099-114, Ref. 10.

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TEST SPECIMEN

Each of the eight sets of the main rotor retention components tested consisted of one 206-010-105-3 strap assembly, one 206-010-123-1 pin and one 206-010-155-7 or 206HA86-1 fitting. The -155-7 fitting was replaced by the 206HA86-1 fitting for the last four sets of the components.

The 206-010-105-3 strap assembly, Ref. 3, shown in Fig. 1, is made of AM-355 stainless steel wires of 0.0058 to 0.0062 inch in diameter wrapped around two end spools set at 9.50 inches apart. The spools are made out of stainless steel which are heat treated to a tensile strength of 180,000 to 200,000 psi. The wire material has a tensile strength of 440,000 psi and is wound in 46 layers with 179 wires per layer bonded with urethane rubber per Bendix ES-1170. The rubber impregnation is done such that the final belt and spool width is 1.199/1.197 inches and the depth of each belt at the center is 0.442/0.412 inch. At each spool a 0.005 inch thick teflon buffer is bonded between the spool and the bonded wire belt. The inboard spool has a pin hole of 0.7505/0.7500 inch in diameter. The outboard spool has a bolt hole of 0.8755/0.8750 inch in diameter.

The 206-010-123-1 pin, shown in Fig. 2, is made out of AISI 4140 steel and is heat treated to a tensile strength of 180,000 - 200,000 psi. The pin is 0.7495/0.7485 inch in diameter and is 2.290 inches long. The ends of the pin are chamfered to 0.060 X 45 degrees.

The 206-010-155-7 strap fitting, shown in Fig. 3, is made out of SAE 4340 steel and heat treated to a tensile strength of 180,000 to 200,000 psi. The -155-7 fitting is essentially cylindrical in shape with a diameter of 2.435/2.438 inches, and has a length of 1.575 inches. At one end it has a flange 0.425 inch long and 2.845 inches in diameter. The outer edge of the flange is chamfered 0.100 x 45 degrees. At the opposite end, the fitting ends in a pair of tangs, which has sides at 45 degrees to the axis of the fitting and is 0.785/0.815 inches long. There is a rectangular cavity through the center of the fitting. At the tang-end of the fitting there is a 0.7500/0.7505 diameter pin hole at 0.785/0.815 inch from

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the end and runs perpendicular to the axis of the fitting. The inboard end of the -105-3 strap assembly fits between the tangs and is located in position by the -123-1 strap retaining pin.

The modification of the -155-7 fitting specified by EO206HES1818 consisted of increasing the fitting tang corner radii, Ref. 11, and shot peening the reworked area.

The 206HA86-1 strap fitting, shown in Fig. 4, is essentially same as the -155-7 fitting except for the 45 degree sides of the tangs. These two cuts are eliminated to form a cylindrical fitting which is 1.575 inches long.

Conformity of Test Specimen

All of the eight -105-3 strap assemblies, ten -123-1 pins and four each of the -155-7 and 206HA86-1 fittings were subjected to conformity inspection prior to test. During the inspection, none of the parts were found to have any deviations from the production drawings. The Bell and FAA Conformity Reports are presented on page 35 through 48.

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TEST LOADS

The magnitudes of the fatigue test loads as specified in Ref. 2, were based on reference loads calculated for various conditions of operation of the Model 206A-1/OH-58A helicopter. The axial load of 44,000 pounds represents the centrifugal force on the strap assembly and the other components at the redline rotor speed of 390 rpm. The oscillatory twist of ± 14 degrees is the result of the constantly varying angle of attack of the blade which occurs during normal helicopter operation. The mean strap-twist angle used in testing was 20 degrees.

The repeated axial loading, also called as the start-stop loading, corresponds to the main rotor starting and stopping during the operational life of the helicopter. The axial load was oscillated from 0 to 44,000 pounds, which corresponds to the maximum main rotor centrifugal force acting on the components. The steady twist of 23 degrees applied on the strap assembly during this part of the test corresponds to the maximum obtainable twist at full down collective.

Each test of the main rotor retention components consisted of applying 10,000,000 oscillatory twist cycles, followed by 34,500 start-stop cycles. These were the blocks of cycles required per Ref. 2 to be met without failure of any component in order to justify an increase in service life.

APPARATUS AND METHODFatigue Test Machine

The test machine was designed to test two sets of the main rotor retention component specimens simultaneously. The machine components which mated with production parts were designed to duplicate the respective helicopter parts, in the area of contact, in order to simulate the helicopter installation. The machine is shown in Figs. 6, 7 and 8.

Two sets of straps, fittings and pins were connected in series, Fig. 6. An axial load was applied at one end of the test assembly and reacted at the opposite end. The inboard ends of the two -105-3 straps were set at the desired angles of pretwist and then the straps were subjected to oscillatory angular twist motion by a constant displacement eccentric mechanism at a bearing supported center fitting.

The eccentric drive mechanism for applying the oscillatory twist cycles was driven by V-belts from an electric motor. The test machine applied approximately 1100 oscillatory twist cycles per minute.

Limit switches were positioned on the machine to stop the drive motor in the event of a decrease in axial load, malfunction of a test machine component, or failure of a test specimen. These switches were used to permit unattended operation during the application of the oscillatory twist cycles.

After the -155-7 fitting failures were noted during test No. 1, break wires were installed on the fittings to stop the test machine in case of a fitting failure.

The axial load was applied by a hydraulic cylinder through a bank of elastic shock cord and a splined fitting, Fig. 6. The strap specimens experienced axial shortening as they were twisted. This required axial freedom. This was obtained by the elastic shock cord and guided axially by the splined fitting, which was allowed to slide in its housing. The elastic shock cord bank also eliminated any axial oscillatory load.

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A hydraulic pressure accumulator was used in the hydraulic system to maintain a constant pressure in the cylinder during long unattended periods of operation. After the hydraulic cylinder failed during test Nos. 1 and 2, a lever assembly with a 2:1 mechanical advantage was used in the axial load system to reduce the load on the hydraulic cylinder.

The repeated axial load cycles, simulating rotor start and stop cycles, were applied by alternately applying and releasing the pressure to the hydraulic cylinder. A portable hydraulic test stand was used as a pressure source and a four-way solenoid valve was used in conjunction with an electrical timer to apply and release the pressure to the cylinder. Application of the repeated axial loading was accomplished at approximately 14 cpm. The test was continuously monitored during the application of the repeated axial load cycles.

Each of the eight sets of components tested were subjected to magnaflux and zygo inspection after the 10⁷ twist cycles were completed. They were also required to be subjected to magnaflux and zygo inspection after 13,000, 19,000, 26,000, and 34,500 cycles in start-stop loading. Though, this was accomplished during test Nos. 3 and 4, the inspection during test Nos. 1 and 2 was interrupted due to test machine failures. During test No. 1 inspection was conducted after 13,400 cycles and after 34,568 cycles. During test No. 2 inspection was conducted after 13,411 cycles and after 20,292 cycles when the test machine failed and the test was discontinued due to damaged strap specimen.

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FATIGUE TEST OF THE MAIN ROTOR RETENTION COMPONENTS
USED ON MODEL OH-58A/206A-1 HELICOPTER

Each set of the main rotor retention components tested consisted of one 206-010-105-3 strap assembly, one 206-010-123-1 pin, and one of the 206-010-155-7 fitting or the 206HA86-1 fitting.

The fatigue tests of four sets of components containing the -155-7 fitting, and four sets of components containing the 206HA86-1 fitting were witnessed by the undersigned:

Witnessed and
Approved by:



C. E. Robertson
Army Engineering Systems
Bell Helicopter Company

Witnessed and
Approved by:



G. McLeod, DER SW-261
Fatigue Evaluation Group
Bell Helicopter Company

Date of Test: September 25, 1970 to January 15, 1971.

Test Location: Mechanical Laboratory
Bell Helicopter Company
Fort Worth, Texas

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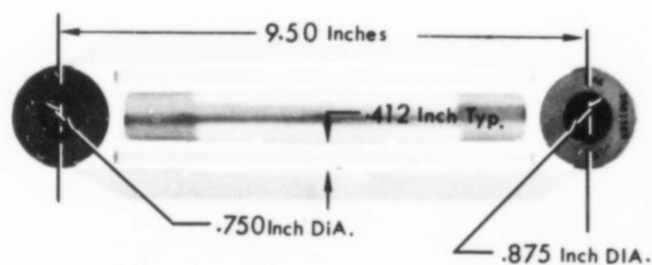


Photo No.
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Photo No.
33611

FIG. 1

206-010-105-3 MAIN ROTOR RETENTION STRAP TEST SPECIMEN

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ROTOR STRAP BOX AND * KNOT & WIRE TIES

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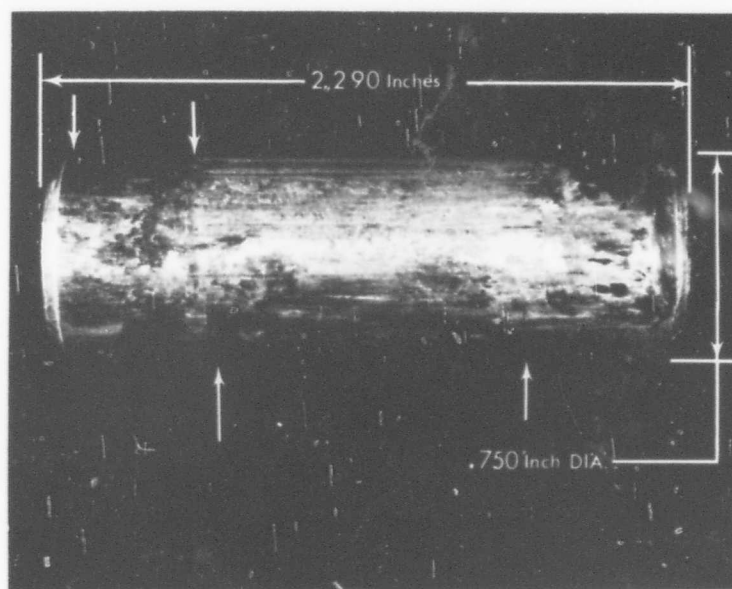


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FIG. 2

206-010-123-1 MAIN ROTOR STRAP RETAINING
PIN TEST SPECIMEN

The photograph shows the retaining pin specimen, S/N Q1-2289, after completing 13,400 start-stop cycles subsequent to 10^7 twist cycles. The arrows enclose the typical areas of fretting.

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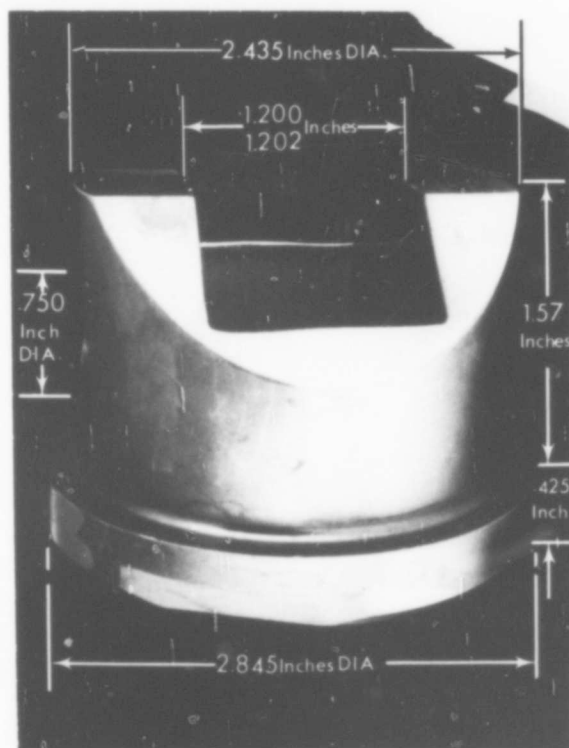


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FIG. 3

206-010-155-7 MAIN ROTOR RETENTION STRAP
FITTING TEST SPECIMEN

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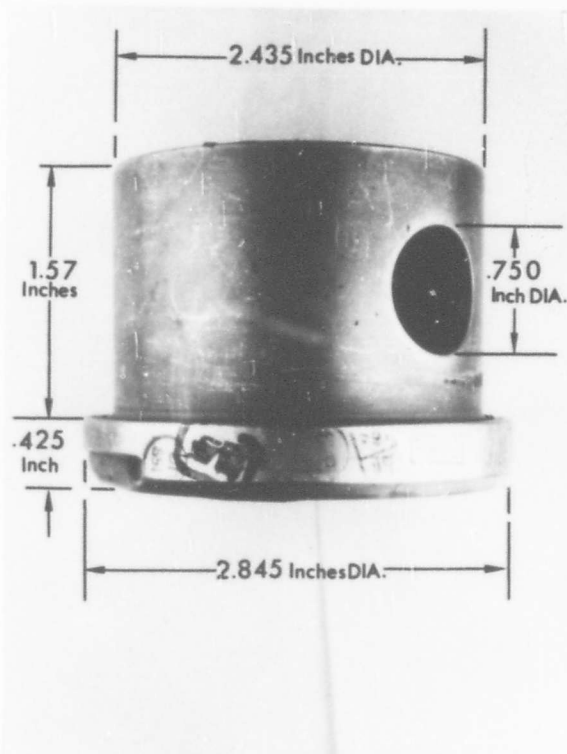


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FIG. 4

206HA86-1 MAIN ROTOR RETENTION STRAP FITTING

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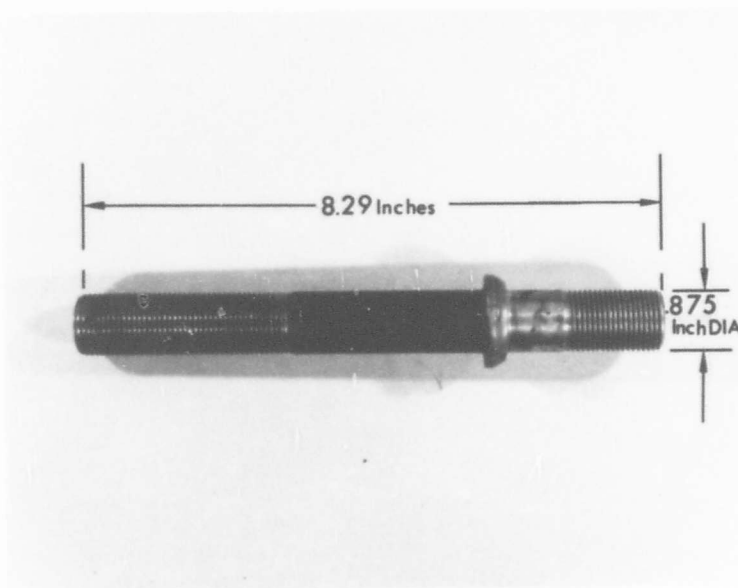


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FIG. 5

206-010-169-1 BOLT USED AS A SUPPORTING PART

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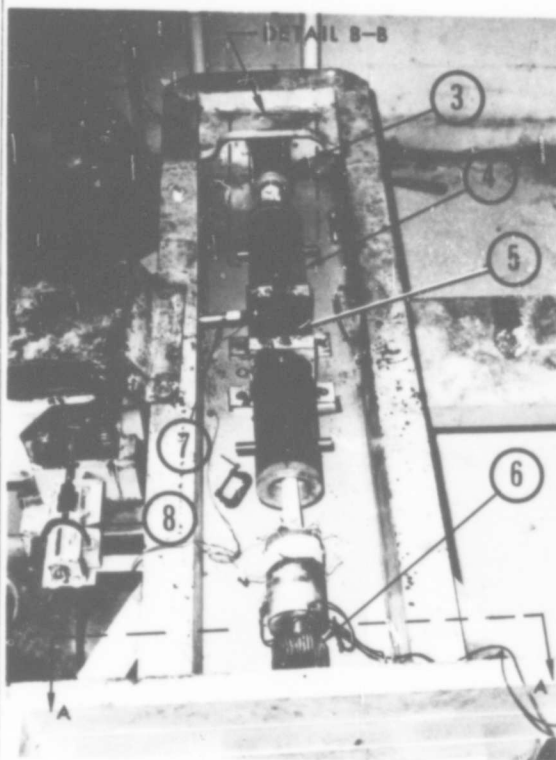
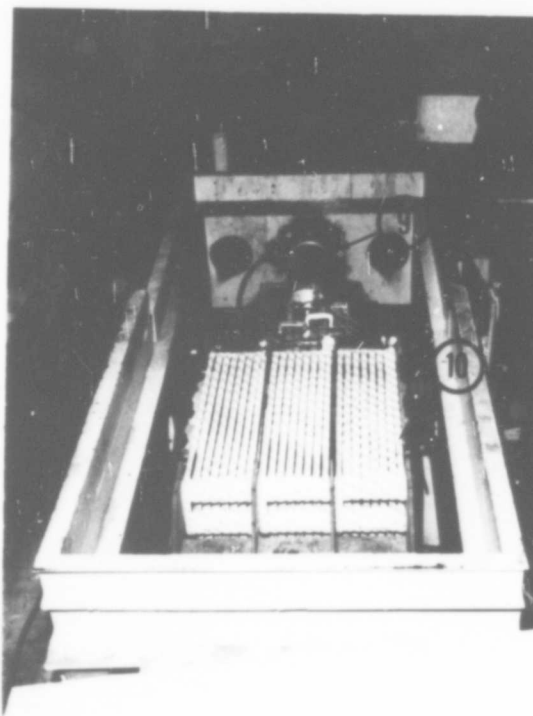


Photo No. 32942



View A-A
Photo No. 32714

FIG. 6

TEST SETUP FOR THE FATIGUE TEST OF THE MAIN ROTOR RETENTION
COMPONENTS USED ON MODEL 206A-1/OH-58A HELICOPTER

Arrows indicate:

1. Housing for electric motor with eccentric drive
2. Test machine frame
3. Housing for retention fitting (2 required)
4. Dummy grip tang housing (2 required)
5. Center slide with clevis end lever
6. Splined shaft to allow axial movement while reacting the applied torsion
7. Eccentric-driven push rod
8. Cycle counter, with 100:1 speed reducer, for measuring oscillatory twist cycles
9. Hydraulic cylinder
10. Elastic shock cord.

Fig. 7 shows detail B-B.

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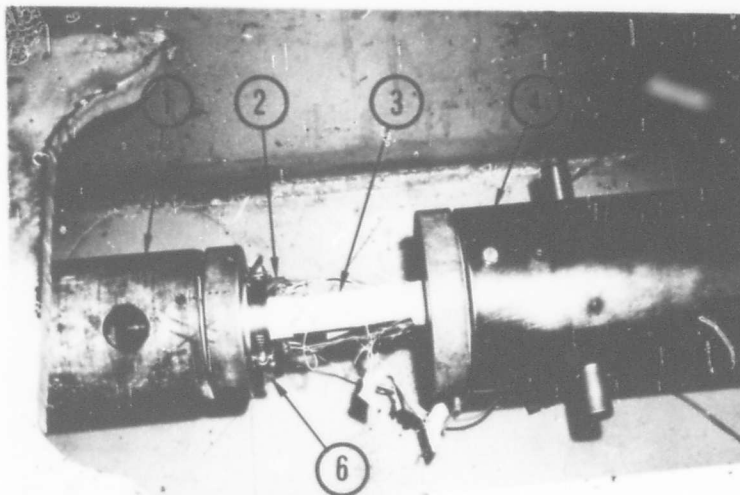


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FIG. 7

DETAILS OF TEST INSTALLATION OF THE MAIN
ROTOR RETENTION COMPONENTS USED ON
MODEL 206A-1/OH-58A HELICOPTER

Arrows indicate:

1. Housing for the 206-010-155-7 retention fitting
2. Retention fitting, P/N 206-010-155-7
3. Retention strap, P/N 206-010-105-3
4. Dummy grip housing
5. Strap retaining bolt, P/N 206-010-169-1
6. Clamp holding the 206-010-123-1 strap retaining pin in place.

This is detail B-B shown in Fig. 6.

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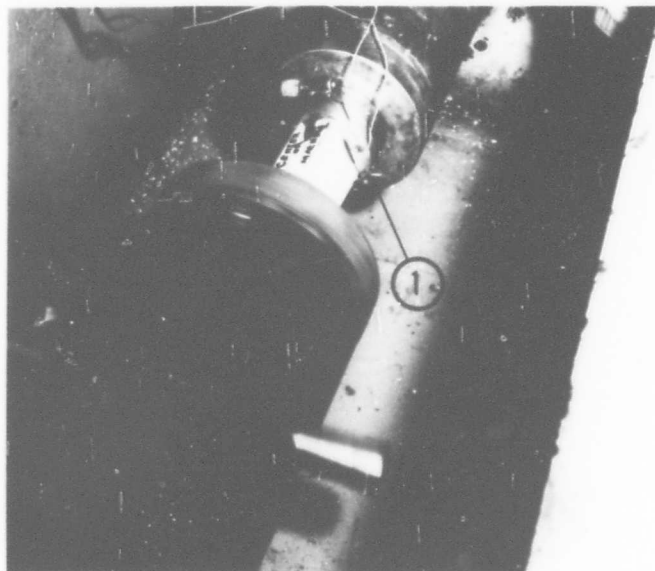


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FIG. 8

DETAILS OF TEST SETUP SHOWING THE INSTALLATION
OF THE 206HA86-1 RETENTION FITTING

The test setup shown is the same as the setup shown in Fig. 7 except the 206-010-155-7 fitting is replaced by the 206HA86-1 fitting.

Arrows indicate:

1. Retention fitting, P/N 206HA86-1.

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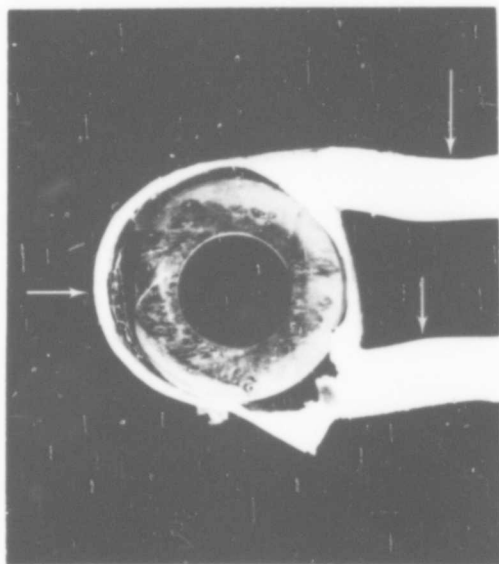
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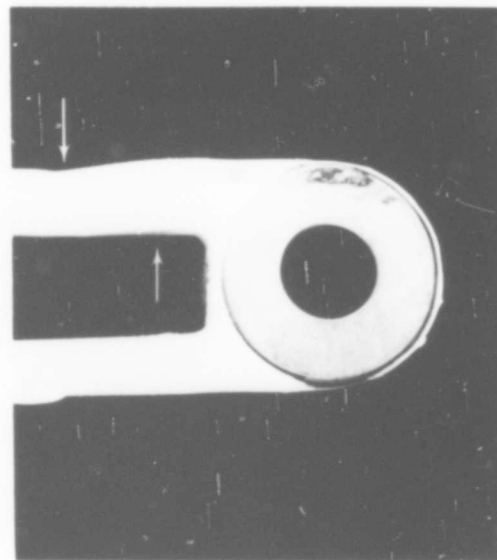
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Outboard End
Photo No. 33289



Inboard End
Photo No. 33288

FIG. 9

TYPICAL DAMAGE OF THE 206-010-105-3 STRAP ASSEMBLY
DUE TO THE TEST MACHINE (HYDRAULIC CYLINDER) FAILURE

Strap shown is specimen No. 3 after 20,292 cycles. Note the fretting of the faces of both the end spools. Arrows indicate the areas of damage due to buckling. Strap specimen No. 4 also had similar damage. The damage on strap specimens Nos. 1 and 2 was similar, but not as severe.

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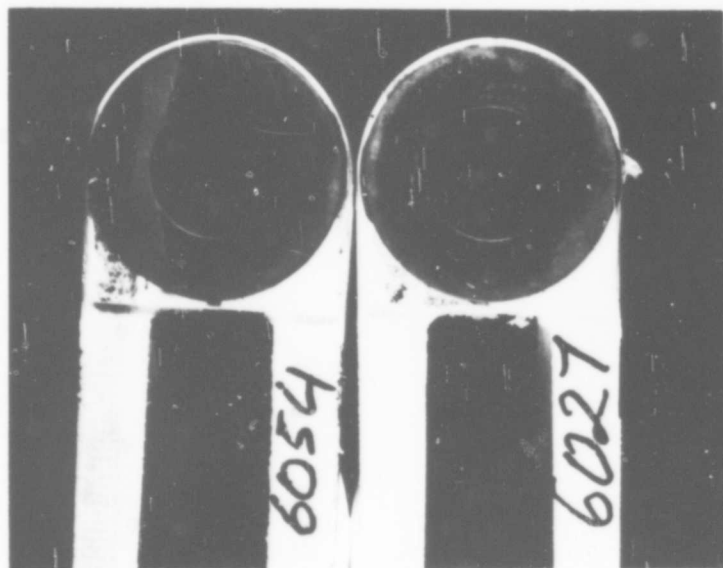


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33450

FIG. 10

TYPICAL CONDITION OF THE 206-010-105-3 STRAP ASSEMBLY
OUTBOARD END SPOOL AREA AFTER 14,000 CYCLES

Straps shown are specimen Nos. 5 and 6 that were used in
test No. 3.

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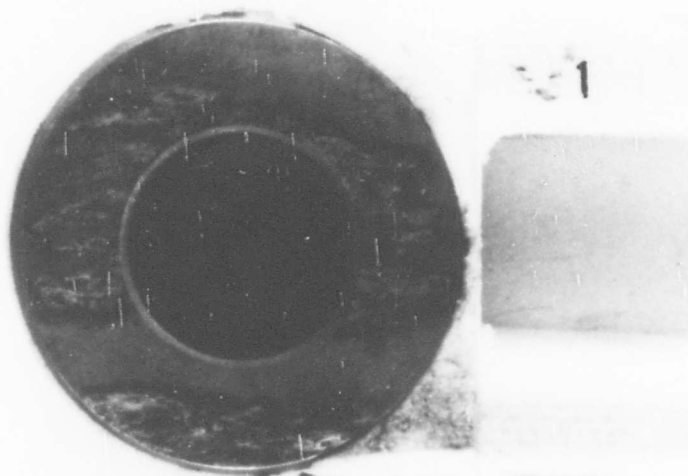


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(a) Outboard End

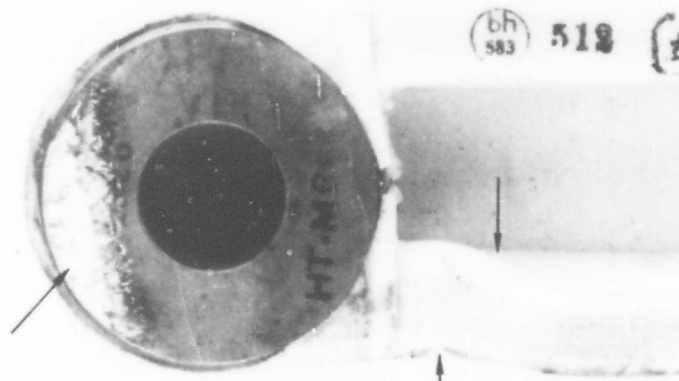


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33820

(b) Inboard End

FIG. 11

TYPICAL CONDITION OF THE 206-010-105-3 STRAP
ASSEMBLY AFTER 72,326 START-STOP CYCLES

The -105-3 strap, S/N 6711, shown was used with 206HA86-1 fitting, ML-4. Arrows indicate the damage at the inboard end due to failure of the mating strap fitting shown in Fig. 15.

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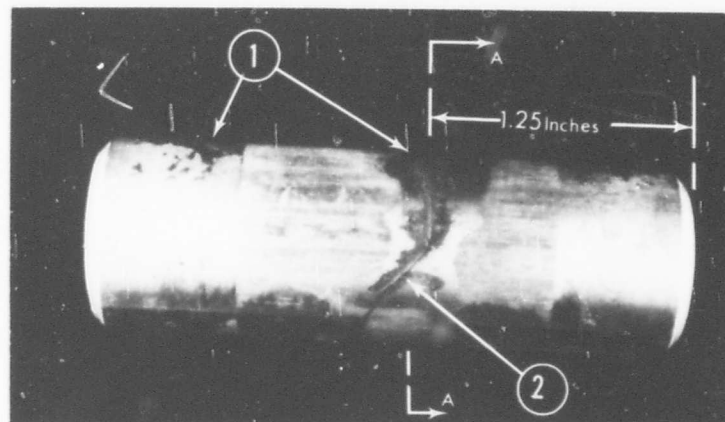


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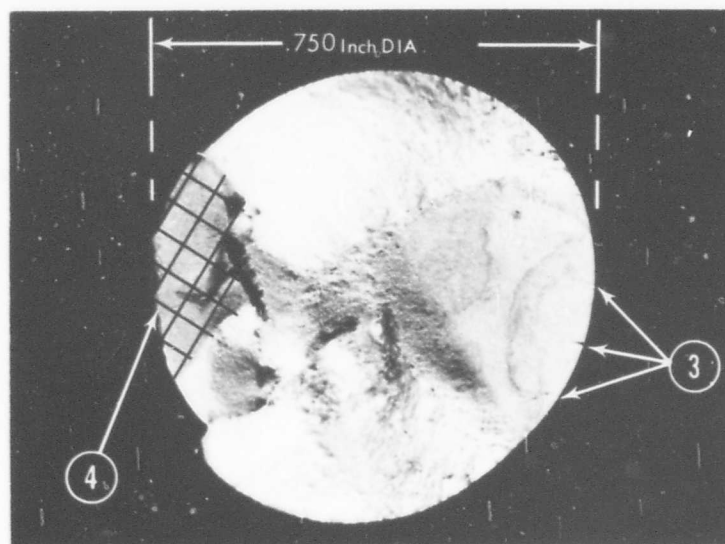


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View A-A (Turned 90° Clockwise)

FIG. 12

FAILURE OF THE 206-010-123-1 RETAINING PIN,
S/N Q1-2382 USED WITH STRAP SPECIMEN NO. 2

Failure was noted during inspection after 34,568 start-stop cycles.

Arrows indicate:

1. Areas of severe fretting
2. Fatigue crack
3. Fatigue origins at areas of severe fretting
4. Area of static failure.

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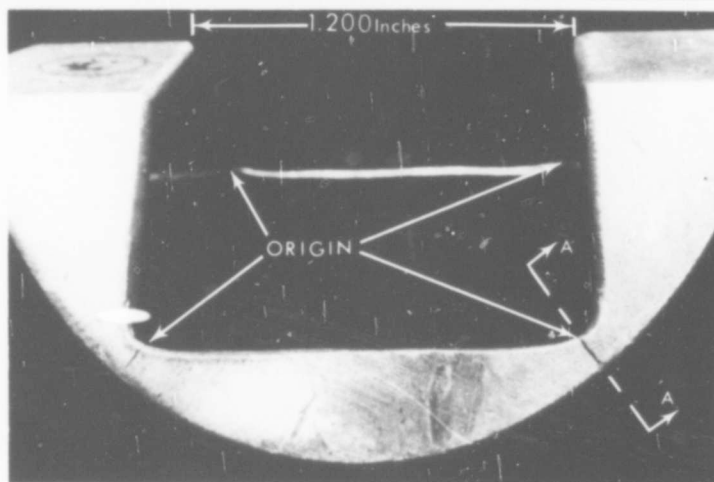


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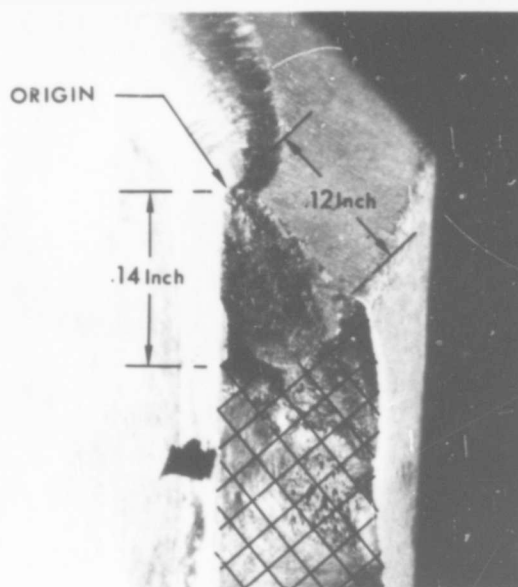


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SECTION A-A

FIG. 13

TYPICAL FAILURE OF THE 206-010-155-7 FITTING

The specimen shown, S/N J11-2088, was used with strap specimen No. 2. Fatigue cracks were discovered during inspection after 13,906 start-stop cycles. The cross-hatched area shown in the lower photograph denotes static failure. See Fig. 3 for overall view of the fitting.

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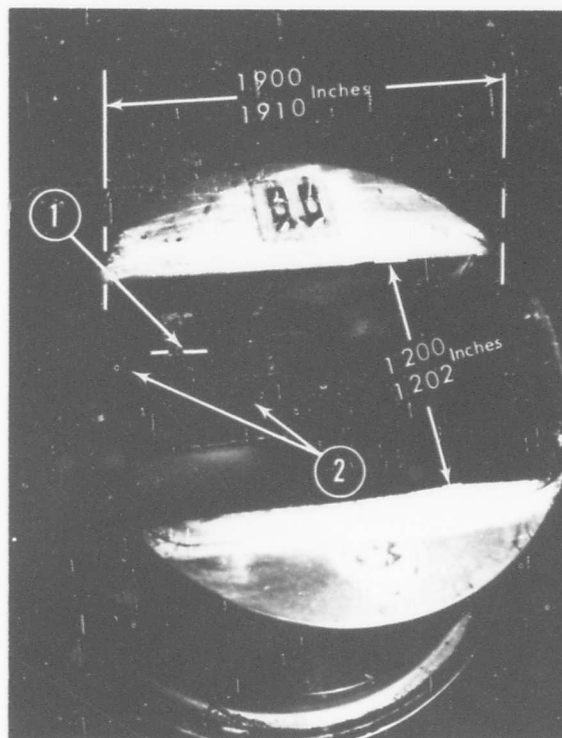


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FIG. 14

TYPICAL CONDITION OF THE 206HA86-1 FITTING
AFTER 14,380 START-STOP CYCLES

Arrows indicate:

1. Typical location of fatigue cracks for Specimen ML-3 used in Set No. 7.
2. Areas of minor fretting

The fitting shown, ML-1, was used with strap specimen No. 5. Fig. 16 shows the details of the failure of specimen ML-3 used with strap specimen No. 7.

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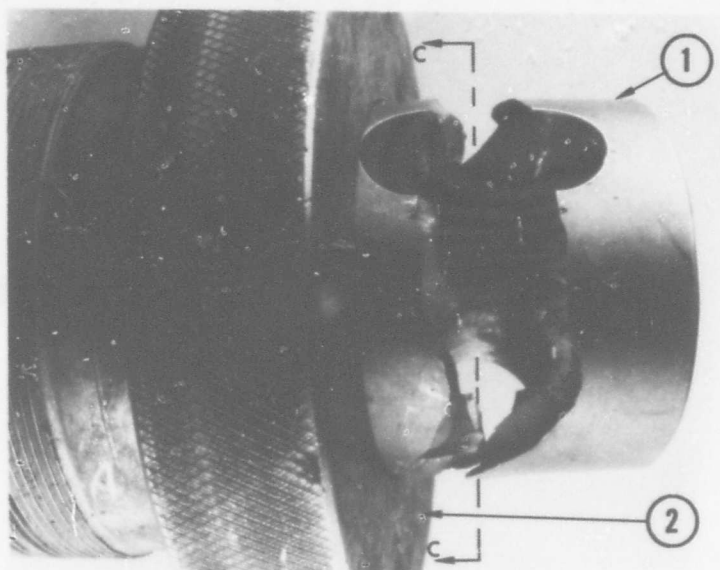


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Outboard →

FIG. 15

FAILURE OF THE 206HA86-1 FITTING, S/N ML-4,
AFTER 72,326 START-STOP CYCLES

Arrows indicate:

1. 206HA86-1 fitting
2. Dummy grip assembly.

The fitting was used in set No. 8. Section C-C is shown
in Fig. 16.

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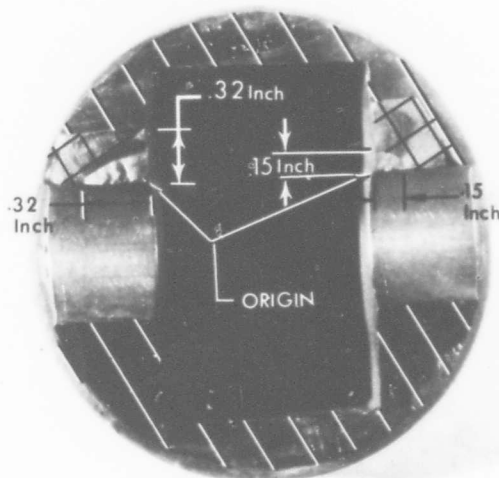


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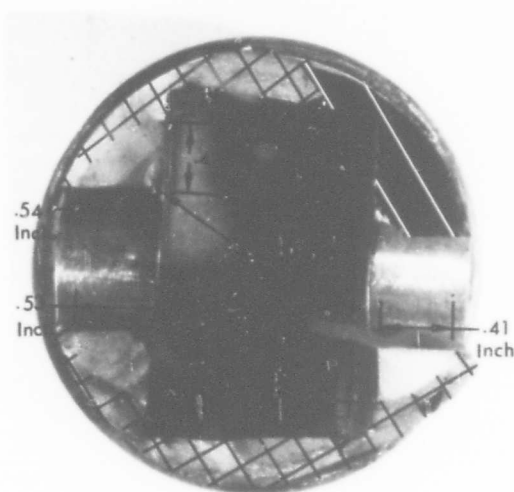


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FIG. 16

DETAILS OF FAILURES OF THE 206HA86-1 FITTINGS,
S/N ML-3 AND ML-4

Top photograph shows failure details of fitting ML-3.
Bottom photograph shows View C-C of fitting ML-4 shown in
Fig. 15. The crosshatched areas indicate the static failure
during the test or the metallurgical examination. The
straight section lines indicate the areas saw cut during
metallurgical examination.

CONFORMITY INSPECTION RECORD

1. TYPE OR PRODUCTION PROJECT NO.

INSTRUCTIONS

(Items not listed are self-explanatory)

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order and date of issuance.

9. Indicate the number of items inspected found to be satisfactory (in conformity and of acceptable workmanship) or unsatisfactory.

10. State the reasons for rejection and what corrective action was taken. Nonconformities in acceptable items will be noted when they are for the prototype product or a test article.

NOTE: Only those items passed by the manufacturer's inspection system should be inspected for conformity.

SP E-0306 KE-2

2. MANUFACTURER

B-11

3. MODEL

200

4. PERIOD COVERED BY THIS REPORT

FROM

TO

5. INSPECTED BY

W. O. AKMS/IRONG DMIR NO. 2008

W. O. Akms/IRONG

10. UNACCEPTABLE CONDITION AND OR CORRECTIVE ACTION TAKEN

6. NOMENCLATURE OF PART INSPECTED

STRAP ASSY

7. DRAWING NO.

204-010-105-3

9. NO. ITEMS

8. DATE AND NO. OF LATEST CHANGE

12-5-68

2-

SN 1447-1455

Delegated By B-2020
8-27-20

Rpt. No. 206-098-164
Page 35

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(Items not listed are self-explanatory)

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order.

9. Indicate the number of items inspected found to be satisfactory (in conformity and of acceptable workmanship) or unsatisfactory.

10. State the reasons for rejection and what corrective action was taken. Nonconformities in acceptable items will be noted when they are for the prototype product or a test article.

NOTE: Only those items passed by the manufacturer's inspection system should be inspected for conformity.

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C FAA AC 69-8291

FAA Form 8100-1 (4-66) FORMERLY FAA FORM 1257

FAA AC 69-8291

0052-039-3000

37

CONFORMITY INSPECTION REPORT

MANUFACTURER

BRUX Corp

MODEL

7-16

DEPT.

34-2-5

BASIC COMPONENT NO.

206-010-105-3

DATE

8-20-70

PAGES

1

INSPECTED BY

[Signature]

	NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING						QUALITY				DIMENSIONAL	INSPECTION STAMP
			LATEST CHANGE ON DRAWING, INCLUDE DATE, UNINCORPORATED E.O'S AFFECTING PART (+)	ARE DRAWINGS ADEQUATE ?	LATEST PLANNING CHANGE	IS PLANNING ADEQUATE ?	ARE TOOLS ADEQUATE ?	MATERIAL	TREATMENT	WORKMANSHIP				
1	57207 PASS	206-010-105	*	+	*	*	*	+	*	*			+	651 BH 436
2		S/Ns. 1447,												
3		1455												
4														
5														
6														
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8														
9														
10														
11														
12														

KEY: AFFIRMATIVE OR SATISFACTORY - +, NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK.

NOTE 1: LIST UNINCORPORATED E.O'S. ON REVERSE SIDE IN CORRESPONDING BLOCK. - +

NOTE 2: ONLY THOSE ITEMS PASSED BY THE MANUFACTURER'S INSPECTION SYSTEM SHOULD BE INSPECTED FOR CONFORMITY.

NOTE 3: LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

(4-000)

MANUFACTURER CORP.		DATE 12-15-70	
MODEL 100	DEPT. 34-25	PAGES 1 of 1	
BASIC COMPONENT NO. 206-010-105		INSPECTED BY J. E. O'NEAL	

CONFORMITY INSPECTION REPORT

NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING						QUALITY CONTROL				DIMENSIONAL	INSPECTION STAMP
		LATEST CHANGE ON DRAWING, INCLUDE DATE, UNINCORPORATED E.O'S AFFECTING PART (+)	ARE DRAWINGS ADEQUATE ?	LATEST PLANNING CHANGE	IS PLANNING ADEQUATE?	ARE TOOLS ADEQUATE?	MATERIAL	TREATMENT	WORKMANSHIP				
1 Strip Assy.	206-010-105-3	10-5-68	*	*	*	*	*	*	*	*	*	519	
2	4-Res.												
3													
4													
5													
6													
7													
8													
9													
10													
11													
12													

KEY: AFFIRMATIVE OR SATISFACTORY - * , NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK,
LIST UNINCORPORATED E.O.'S. ON REVERSE SIDE IN CORRESPONDING BLOCK. - +
NOTE 1: ONLY THOSE ITEMS PASSED BY THE MANUFACTURER'S INSPECTION SYSTEM SHOULD BE INSPECTED FOR CONFORMITY.
NOTE 2: LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

CONFORMITY INSPECTION RECORD

INSTRUCTIONS

(Items not listed are self-explanatory)

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order and date of issuance.
9. Indicate the number of items inspected found to be satisfactory (in conformity and of acceptable workmanship) or unsatisfactory.

10. State the reasons for rejection and what corrective action was taken. Nonconformities in acceptable items will be noted when they are for the prototype product or a test article.

NOTE: Only those items passed by the manufacturer's inspection system should be inspected for conformity.

6. NOMENCLATURE OF PART INSPECTED	7. DRAWING NO.	8. DATE AND NO. OF LATEST CHANGE	9. NO. ITEMS		10. UNACCEPTABLE CONDITION AND/OR CORRECTIVE ACTION TAKEN
			FOUND SAT.	FOUND UNSAT.	
STRAP ASSY TENSION	206-010-105-3	G 12-5-68	4		SN 6005, 6027, 6054, 6025
TORSION MAIN ROTOR					
WASHER, BLADE ROCT. M/R	206-010-154-1	B 7-19-68	6		
WASHER BLADE ROCT. M/R	206-010-153-1	11-27-68	6		MANUFACTURING DATE NOTED PARTS.
			6		ADDED OK. PER
FITTING Retention STRAP M/R	206-010-153-7	D 1-31-69	4		SN 111-2098, 2070, 2111, 2088
RING, BACK UP TENSION	206-010-113-5	B 7-18-68	4		
STRAP RETAINER					
PIN STRAP RETAINING	206-010-123-1	B 7-18-68	6		SN 81-2112, 2382, 2377, 2284
					2289, 2232

EO 206 4A87

FRANCIS HARRIS

CONFORMITY INSPECTION RECORD

1. TYPE OR PRODUCTION PROJECT NO.

INSTRUCTIONS

(Items not listed are self-explanatory)

2. MANUFACTURER

Be 11

3. MODEL

206A

4. PERIOD COVERED BY THIS REPORT

FROM

to

11-6-70	11-9-70
---------	---------

5. INSPECTED BY W. O. ARMSTRONG NMIR NO. 2018

Mr. D. W. D. 4018

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order and date of issuance.

9. Indicate the number of items inspected found to be satisfactory (in conformity and of acceptable workmanship) or unsatisfactory.

•10. State the reasons for rejection and what corrective action was taken. Nonconformities in acceptable items will be noted when they are for the prototype product or a test article.

NOTE: Only those items passed by the manufacturer's inspection system should be inspected for conformity.

Test E-0306HA-87

6. NOMENCLATURE OF PART INSPECTED

7. DRAWING NO.

9. NO. ITEMS

FOUND SAT.	FOUND UNSAT.

8. DATE AND NO.
OF
LATEST CHANGE

10. UNACCEPTABLE CONDITION AND/OR CORRECTIVE ACTION TAKEN

127x

206-016-123-1

7-18-68

4

SN Q12894-2854-2895-2
Q1-2470.

FITTING

206-010-155-7

D
1-21-69

以

SN 51-2600 51-2599-51-2616
51-2614

Delegated 11-6-70

R. H. D.

4 PCS.

MANUFACTURER

BENDIX CORP.

MODEL

206

DEPT.

34/25

BASIC COMPONENT NO.

206-010-105

CONFORMITY INSPECTION REPORT

206H4-NR

DATE

9-1-70

PAGES

ONE OF ONE

INSPECTED BY

J. A. Willis

	NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING						QUALITY CONTROL			
			LATEST CHANGE ON DRAWING, INCLUDE DATE, UNINCORPORATED E.O.'S AFFECTING PART (+)	ARE DRAWINGS ADEQUATE ?	LATEST PLANNING CHANGE	IS PLANNING ADEQUATE ?	ARE TOOLS ADEQUATE ?	MATERIAL	TREATMENT	WORKMANSHIP	DIMENSIONAL	INSPECTION STAMP
1	STRAP ASSY.	206-010-105-3	'G' 12-5-68	*	3-5-69	*	*	*	*	*	*	(511) (523)
2		4 Pcs.										
3												
4												
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9												
10												
11												
12												

KEY:

AFFIRMATIVE OR SATISFACTORY - * , NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK,
LIST UNINCORPORATED E.O.'S, ON REVERSE SIDE IN CORRESPONDING BLOCK. - +

NOTE 1:

ONLY THOSE ITEMS PASSED BY THE MANUFACTURER'S INSPECTION SYSTEM SHOULD BE INSPECTED FOR CONFORMITY.

NOTE 2:

LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

7/8 95536 RLV 363

6 PC

MANUFACTURER		DATE		PAGES		ONE OF ONE		INSPECTED BY															
CRESCENT PRECISION PROD.		9-1-70		ONE OF ONE		ONE OF ONE		J. Williams															
MODEL		34/25		206		206-C10-123		206-C10-123															
BASIC COMPONENT NO.		206-C10-123		206-C10-123		206-C10-123		206-C10-123															
1	NOMENCLATURE OF PART INSPECTED	2	DRAWING (PART) NUMBER	3	LAST CHANGE ON DRAWING, INCLUDE DATE, UNINCORPORATED E.O'S AFFECTING PART (+)	4	ARE DRAWINGS ADEQUATE?	5	LATEST PLANNING CHANGE	6	IS PLANNING ADEQUATE?	7	ARE TOOLS ADEQUATE?	8	MATERIAL	9	TREATMENT	10	WORKMANSHIP	11	DIMENSIONAL	12	INSPECTION STAMP
1	PIN	206-C10-123-1	B' 7-18-68	*	3-10-69	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	41	
2		6 Pcs.																					
3																							
4																							
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8																							
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KEY: AFFIRMATIVE OR SATISFACTORY - +, NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK.

LIST UNINCORPORATED E.O'S. ON REVERSE SIDE IN CORRESPONDING BLOCK. - +

NOTE 1: ONLY THOSE ITEMS PASSED BY THE MANUFACTURER'S INSPECTION SYSTEM SHOULD BE INSPECTED FOR CONFORMITY.

NOTE 2: LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

MANUFACTURER		DEPT.		DATE											
MODEL		DEPT.		PAGES											
BASIC COMPONENT NO.		DEPT.		INSPECTED BY											
206		34/25		11-2-70											
TEST P.0206HA-87				J.C. Pruitt											
R-0206HA-87															
NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING						QUALITY CONTROL				DIMENSIONAL	INSPECTION STAMP		
		1	2	3	4	5	6	7	8	9	10			11	
1 SNAP Assy	206-010-105-3														
2 PIN, 4 Pcs	206-010-123-1														
3 FITTING, 4 Pcs	206-010-155-7														
4 BOLT	206-010-169-1														
5															
6															
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9															
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KEY: AFFIRMATIVE OR SATISFACTORY - +, NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK, LIST UNINCORPORATED E.O.'S. ON REVERSE SIDE IN CORRESPONDING BLOCK. - +

NOTE 1: ONLY THOSE ITEMS PASSED BY THE MANUFACTURER'S INSPECTION SYSTEM SHOULD BE INSPECTED FOR CONFORMITY.

NOTE 2: LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

7878 88838 REV 245

4 Pcs.

MANUFACTURER AUTOMATION IND. INC.		DATE 9-1-70		CONFORMITY INSPECTION REPORT													
MODEL 206		DEPT. 34/25		PAGES ONE OF ONE		INSPECTED BY G. Williams											
BASIC COMPONENT NO. 206-010-155																	
NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING						QUALITY CONTROL						INSPECTION STAMP			
		1	2	3	4	5	6	7	8	9	10	11	12				
1 Fitting	206-010-155-7																
1 ASSY	4 Pcs.																
2																	
3																	
4																	
5																	
6																	
7																	
8																	
9																	
10																	
11																	
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KEY: AFFIRMATIVE OR SATISFACTORY - * , NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK.

NOTE 1: LIST UNINCORPORATED E.O.'S. ON REVERSE SIDE IN CORRESPONDING BLOCK. - 4

NOTE 2: LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

1. TYPE OF PRODUCTION PROJECT NO.

(Items not listed are self-explanatory)

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order and date of issuance.

9. Indicate the number of items inspected found to be satisfactory to conformity and of acceptable workmanship or unsatisfactory.

10. State the reasons for rejection and what corrective action was taken. Nonconformities in acceptable items will be noted when they are for the prototype product or a test article.

NOTE: Only those items passed by the manufacturer's inspection system should be accepted for conformity.

Dear Sir,

6. NOMENCLATURE OF PART INSPECTED

7. DRAWING NO. 11

9. DATE AND NO. OF LATEST CHANGE

9. NO. ITEMS	FOUND	UNSAT.
--------------	-------	--------

10. UNACCEPTABLE CONDITION AND/OR CORRECTIVE ACTION TAKEN

Retention Strip Fitting
F.00D47931 S

Test
206 H.9 S6-1

12-71-70

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----

Notes

SAME as SOL-010-153-7. Fishy ass
excepted as noted on SOL-010-153-6
SOL-010-153-8 and dated 1-21-69

Rpt. No. 206-098-164
Page 45

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CONFORMITY INSPECTION RECORD

INSTRUCTIONS

(Items not listed are self-explanatory)

8. Indicate the latest drawing change number or letter noted on the drawing, together with the date. When pertinent, indicate the latest engineering change or change order and date of issuance.

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1. TYPE OR PRODUCTION PROJECT NO.

2. MANUFACTURE

3. MODEL

4. PERIOD COVERED BY THIS REPORT

FROM	TO
1	2
3	4
5	6
7	8
9	10
11	12
13	14
15	16
17	18
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79	80
81	82
83	84
85	86
87	88
89	90
91	92
93	94
95	96
97	98
99	100

5. INSPECTED BY DDMR

6. NOMENCLATURE OF PART INSPECTED

7. DRAWING NO.

8. DATE AND NO.
OF
LATEST CHANGE

9. NO. ITEMS	FOUND	FOUND
	SAT.	UNSA

10. UNACCEPTABLE CONDITION AND/OR CORRECTIVE ACTION TAKEN

Bolt, steel retaining

206-010-169-1

3-7-69

6

FAA Form 8100-1 (4-66) FORMERLY FAA FORM 1257

Page 641

0052-039-3000

5 Pcs.

MANUFACTURER

AUTOMATION IND. INC.

MODEL

206

DEPT.

34/25

BASIC COMPONENT NO.

206-Q10-169

CONFORMITY INSPECTION REPORT

DATE

9-8-70

PAGES

ONE OF ONE

INSPECTED BY

C. W. Williams

206-Q10-169-1		NOMENCLATURE OF PART INSPECTED	DRAWING (PART) NUMBER	STATUS OF DRAWING & PLANNING								QUALITY CONTROL				INSPECTION STAMP
1	2			3	4	5	6	7	8	9	10	11	12			
1	BOLT	206 Q10-169-1	C' 3-7-69	*	7-7-70	*	*	*	*	*	*	*	*	44		
2		6 Pcs.														
3																
4																
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12																

KEY:

AFFIRMATIVE OR SATISFACTORY - * , NEGATIVE OR UNSATISFACTORY - X, NOT REQUIRED OR NOT APPLICABLE - LEAVE BLANK.
 LIST UNINCORPORATED E.O.'S, ON REVERSE SIDE IN CORRESPONDING BLOCK. - 4

NOTE 1:

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NOTE 2:

LIST REMARKS ON BACK NUMERICALLY FOR ALL UNSATISFACTORY CONDITIONS.

BY R. Amancharla

CHECKED J. K. Sen

BELL HELICOPTER COMPANY
POST OFFICE BOX 482 • FORT WORTH 1 TEXAS

MODEL OH-58A/ PAGE 49
206A-I
RPT 206-098-164

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